

# UNCLASSIFIED

AD NUMBER
AD818407
NEW LIMITATION CHANGE
TO Approved for public release, distribution unlimited
FROM Distribution authorized to U.S. Gov't. agencies and their contractors; Critical Technology; AUG 1967. Other requests shall be referred to Air Force Weapons Lab., AFSC, Kirtland AFB, NM.
AUTHORITY
AFWL ltr, 30 Nov 1971

THIS PAGE IS UNCLASSIFIED

AFWL-TR-67-75

AFWL-TR  
67-75

AD818407

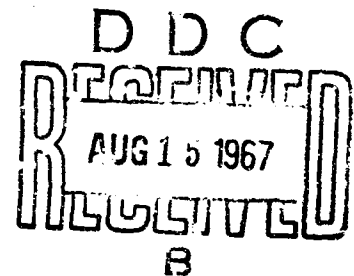


## ATMOSPHERIC MODELS FOR USE IN HYDRODYNAMIC COMPUTER CODES

Jeremiah U. Brackbill  
Lieutenant USAF

Edmund A. Nawrocki  
Captain USAF

William A. Whitaker  
Major USAF



TECHNICAL REPORT NO. AFWL-TR-67-75

August 1967

AIR FORCE WEAPONS LABORATORY  
Research and Technology Division  
Air Force Systems Command  
Kirtland Air Force Base  
New Mexico

Research and Technology Division  
AIR FORCE WEAPONS LABORATORY  
Air Force Systems Command  
Kirtland Air Force Base  
New Mexico

When U. S. Government drawings, specifications, or other data are used for any purpose other than a definitely related Government procurement operation, the Government thereby incurs no responsibility nor any obligation whatsoever, and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise, as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

This report is made available for study with the understanding that proprietary interests in and relating thereto will not be impaired. In case of apparent conflict or any other questions between the Government's rights and those of others, notify the Judge Advocate, Air Force Systems Command, Andrews Air Force Base, Washington, D. C. 20331.

This document is subject to special export controls and each transmittal to foreign governments or foreign nationals may be made only with prior approval of AFWL (WLRT), Kirtland AFB, NM, 87117. Distribution is limited because of the technology discussed in the report.

DO NOT RETURN THIS COPY. RETAIN OR DESTROY.

ATMOSPHERIC MODELS FOR USE IN HYDRODYNAMIC COMPUTER CODES

Jeremiah U. Brackbill  
Lieutenant      USAF

Edmund A. Nawrocki  
Captain      USAF

William A. Whitaker  
Major      USAF

TECHNICAL REPORT NO. AFWL-TR-67-75

This document is subject to special export controls and each transmittal to foreign governments or foreign nationals may be made only with prior approval of AFWL (WLRT), Kirtland AFB, NM, 87117. Distribution is limited because of the technology discussed in the report.

FOREWORD

This research was performed under Program Element 7.60.06.01.D, Project 5710, Task 571007K, Subtask 07.002, and was funded by the Defense Atomic Support Agency (DASA).

Inclusive dates of research were 1 August 1964 to 1 September 1964. The report was submitted 24 July 1967 by the Air Force Weapons Laboratory Project Officer, Lt Jeremiah U. Brackbill (WLRT).

This technical report has been reviewed and is approved.

*Jeremiah U. Brackbill*  
JEREMIAH U. BRACKBILL  
Lt, USAF  
Project Officer

*George R. Spillman*  
GEORGE R. SPILLMAN  
Major, USAF  
Chief, Theoretical Branch

*Claude K. Stambaugh*  
CLAUDE K. STAMBAUGH  
Colonel, USAF  
Chief, Research Division

ABSTRACT

(Distribution Limitation Statement No. 2)

A hydrostatically stable atmospheric model is necessary to perform theoretical calculations of hydrodynamic motion in the atmosphere, on a digital computer. This report presents three such models developed at the Air Force Weapons Laboratory for use in its hydrodynamic computer codes. One is for the annual mean temperate atmosphere ( $45^{\circ}$  N latitude); one for the annual mean tropical atmosphere ( $15^{\circ}$  N latitude); and one for the summer subarctic atmosphere ( $60^{\circ}$  N latitude). The models are presented herein in tabular form and as FORTRAN subroutines which could be placed directly into any hydrodynamic computer code. For a given altitude (cm), the subroutines return a pressure (dynes/cm<sup>2</sup>), density (gms/cm<sup>3</sup>), specific internal energy (ergs/gm), temperature ( $^{\circ}$ K), and  $(\gamma - 1)$ . The pressures and densities agree with tabulated values to at least 1 part in  $10^8$  and temperatures to at least 1 part in 100. The atmospheres experience an acceleration of no more than 3 parts in  $10^3$  in a first order finite difference scheme with a zone size of 1 kilometer, the worst case.

## CONTENTS

<u>Section</u>	<u>Page</u>
I INTRODUCTION	1
II DERIVATION OF THE MODELS	3
Conditions and Assumptions	3
Calculations	5
Transition Region at 90 km for the Tropical Atmospheric Model	6
III APPLICATIONS	8
IV RESULTS	10
V CONCLUSIONS	17
APPENDIX	19
REFERENCES	25
DISTRIBUTION	26

## TABLES

<u>Table</u>		<u>Page</u>
I	Difference in Atmospheric Data for the Altitude 90 km Given by References 1 and 2	6
II	Defining Properties of the Annual Mean Temperate Atmospheric Model (45° N Latitude)	11
III	Defining Properties of the Annual Mean Tropical Atmospheric Model (15° N Latitude)	12
IV	Defining Properties of the Summer Subarctic Atmospheric Model (60° N Latitude)	13
V	Differences between Calculated and Tabulated Molecular Scale Temperatures in the Temperate Atmospheric Model	14
VI	Differences between Calculated and Tabulated Molecular Scale Temperatures in the Tropical Atmospheric Model	15
VII	Differences between Calculated and Tabulated Molecular Scale Temperatures in the Subarctic Atmospheric Model	16



## SECTION I

## INTRODUCTION

The Air Force Weapons Laboratory is engaged in research on the phenomenology of atmospheric nuclear weapons detonations. This research consists of numerical experiments--theoretical calculations of various yield-altitude detonations--performed on large memory, high-speed computers. These calculations are made by a series of large, complex, computer codes that enable prediction, from essentially first principles, of the phenomenology from microseconds to minutes after a detonation.

Three main codes are used: SPUTTER, a one-dimensional radiation transport Lagrangian hydrodynamic code; SAP, a one-dimensional Lagrangian hydrodynamic code; and SHELL, a two-dimensional Eulerian hydrodynamic code that also has the capability of doing radiation diffusion. The first, SPUTTER, takes the radiative output directly from weapons design calculations, deposits the energy in air, and calculates the radiative and hydrodynamic growth of the fireball to a time of about 1 second. It uses a multifrequency transport scheme involving typically 20 frequency groups. The output of this code is used as input to SAP, which calculates the hydrodynamic expansion of the shock wave at various angles to the horizontal. The output of SPUTTER is also used as input to SHELL, which calculates fireball growth and rise to late times.

These codes, or any hydrodynamic code in general, which perform hydrodynamic calculations in a real atmosphere, need an atmospheric model that is stable in a  $R^{-2}$  gravity field; otherwise, the numerical integration of the hydrodynamic equations will result in fictional vertical velocity components.

This report describes three stable atmospheric models developed at the Air Force Weapons Laboratory. The first model is based on data in reference 1 for an annual mean, temperate atmosphere (45° N latitude) for altitudes from sea level to 700 kilometers. The second is based on data in reference 2 for an annual mean, tropical atmosphere (15° N latitude) for altitudes from sea level

to 90 kilometers and reference 1 for altitudes from 90 to 700 kilometers. The third is based on data in reference 3 for a summer subarctic atmosphere (60° N latitude) for altitudes from sea level to 90 kilometers and reference 1 for altitudes from 90 to 700 kilometers

The Appendix contains a FORTRAN subroutine for the models.

## SECTION II

### DERIVATION OF THE MODELS

#### 1. Conditions and Assumptions

The molecular scale temperature is the defining property of the US Standard Atmosphere, 1962 (Ref. 1). It is defined by the relationship

$$T_m(z) = \frac{M_0}{M(z)} T(z) \quad (1)$$

where  $T_m(z)$  = molecular scale temperature at altitude  $z$   
 $T(z)$  = absolute temperature at altitude  $z$   
 $M(z)$  = molecular weight of air at altitude  $z$   
 $M_0$  = molecular weight of air at sea level

The variation of the molecular scale temperature is defined as a series of connected segments linear in geopotential altitude to 90 kilometers and in geometric altitude above 90 kilometers (Ref. 1). Therefore, we divide the temperate, tropical, and subarctic models into 21, 22, and 23 altitude groups respectively from sea level to 700 kilometers and assume a linear molecular scale temperature variation with altitude within each altitude group. This variation has the form

$$T_m(z) = T_m(z_i) + (L_i)(z - z_i) \quad (2)$$

where  $z_i$  = the base altitude of the  $i$ -th altitude group  
 $L_i$  = the molecular scale temperature gradient over the  $i$ -th altitude group

$$= \frac{T_m(z_{i+1}) - T_m(z_i)}{z_{i+1} - z_i}$$

We also assume the atmosphere behaves like an ideal gas in which case

$$\rho(z) = \frac{M(z)p(z)}{RT(z)} \quad (3)$$

where  $\rho(z) \equiv$  the density at altitude  $z$   
 $p(z) \equiv$  the pressure at altitude  $z$   
 $R \equiv$  the universal gas constant

Finally, we require the atmospheric models to satisfy the condition of stability given by the hydrostatic equation

$$\frac{d[p(z)]}{dz} = -\rho(z)g(z) \quad (4)$$

where  $g(z) \equiv$  the acceleration due to gravity at altitude  $z$   

$$= \frac{g_0 a^2}{(a+z)^2} \quad (5)$$

$g_0 \equiv$  the acceleration due to gravity at sea level  
 $a \equiv$  the radius of the earth

By combining equations 1 through 4, the hydrostatic equation becomes

$$\frac{d[p(z)]}{p(z)} = - \frac{g_0 M_0 a^2}{R} \frac{dz}{(a+z)^2 \left[ T_m(z_1) + (L_1)(z-z_1) \right]} \quad (6)$$

Integration of equation 6 from  $z_1$  to  $z$  results in the final form, which is used to calculate pressures in each altitude group.

$$\ln \frac{p(z)}{p(z_1)} = - \frac{g_0 M_0 a^2}{\left[ T_m(z_1) - (L_1)(a+z_1) \right]^2 R} \left\{ \frac{\left[ T_m(z_1) - (L_1)(a+z) \right] (z-z_1)}{(a+z)(a+z_1)} + L_1 \ln \left[ \frac{a+z_1}{a+z} \frac{T_m(z_1) + (L_1)(z-z_1)}{T_m(z_1)} \right] \right\} \quad (7)$$

## 2. Calculations

To calculate the molecular scale temperatures,  $T_m(z_i)$ , and the molecular scale temperature gradients,  $L_i$ , which define each atmospheric model, we take the pressures listed in references 1, 2, and 3 corresponding to the base altitude of each altitude group and the molecular scale temperatures as defined by equation 2 to be constants. With  $p(z_{i+1})$ ,  $p(z_i)$ ,  $T_m(z_i)$ ,  $a$ ,  $g_0$ ,  $R$ , and  $M_0$  known, equation 7 becomes

$$\ln \frac{p(z_{i+1})}{p(z_i)} = - \frac{g_0 M_0 a^2}{[T_m(z_i) - (L_i)(a+z_i)]^2 R} \left\{ \frac{[T_m(z_i) - (L_i)(a+z_i)](z_{i+1}-z_i)}{(a+z_{i+1})(a+z_i)} + L_i \ln \left[ \frac{a+z_i}{a+z_{i+1}} \frac{T_m(z_i) + (L_i)(z_{i+1}-z_i)}{T_m(z_i)} \right] \right\} \quad (8)$$

which is solved by an appropriate iterative technique to find that molecular scale temperature gradient,  $L_i$ , which will satisfy equation 8 and thus, satisfy the condition of hydrostatic stability for the  $i$ -th group. Then the molecular scale temperature corresponding to the base altitude of the next altitude group becomes

$$T_m(z_{i+1}) = T_m(z_i) + (L_i)(z_{i+1}-z_i) \quad (9)$$

where  $L_i$  is the gradient just calculated. Then the calculation proceeds to the next altitude group where the exact procedure is repeated. This procedure is repeated until the molecular scale temperature and gradient have been calculated for all altitude groups.

The calculation begins at sea level for which we take the molecular scale temperature as listed in references 1, 2, and 3. (This temperature can be thought of as an "initial condition." All other temperatures are defined by the gradients obtained from the solution of equation 8 and equation 9.) Solution of equation 8 provides  $L_1$  which is used in equation 9 to obtain  $T_2$ . Using  $T_2$ , equation 8 gives  $L_2$ , which in turn by equation 9 gives  $T_3$ , and so forth.

We repeat the above iteration for each model using the appropriate data for  $p(z_1)$ ,  $T_m(0)$ , and  $g_0$  as given by the references.

### 3. Transition Region at 90 km for the Tropical Atmospheric Model

We used the procedure outlined above to calculate the defining properties of all three atmospheric models. However, in the case of the tropical model, the arithmetic error between calculated and tabulated temperatures increased in magnitude and alternated in sign with increasing altitudes above 90 km. This result was caused by the poor match of data at 90 km provided by references 1 and 2. Table I shows the difference in data provided by the two references at 90 km.

Table I

DIFFERENCE IN ATMOSPHERIC DATA FOR THE ALTITUDE  
90 km GIVEN BY REFERENCES 1 AND 2

	<u><math>p(\text{dynes/cm}^2)</math></u>	<u><math>\rho(\text{gm/cm}^3)</math></u>	<u><math>T_m(^{\circ}\text{K})</math></u>
Ref 1	1.6438	$3.1700 \times 10^{-9}$	180.65
Ref 2	1.8620	$3.5224 \times 10^{-9}$	184.15

Therefore, we created a transition region between 90 and 110 km to effect a smooth transition from the data in reference 2 (0 to 90 km) to the data in reference 1 (90 to 700 km). We did this by replacing the two altitude groups from 90 to 100 km and from 100 to 110 km by two groups from 90 km to an altitude,  $z$ , to be determined, and from  $z$  to 110 km.

We determined the altitude,  $z$ , in the following manner. First, the basic procedure outlined in section II-2 was used to calculate the molecular scale temperatures and gradients for the altitude groups from 0 to 90 km, using the data in reference 2. Next, we assumed that the isothermal region from 80.13 to 90 km actually extends from 80.13 km to the altitude,  $z$ ; that is,  $T_m(80.13) = T_m(90) = T_m(z)$  or  $L(80.13 \rightarrow z) = 0$ . Then we calculated the altitude,  $z$ , by iteration according to the analysis below.

Since

$$\ln \left[ \frac{p(110)}{p(90)} \right] = \ln \left[ \frac{p(z)}{p(90)} \right]_{(L=0)} + \ln \left[ \frac{p(110)}{p(z)} \right]_{(L=0)} \quad (10)$$

we have an equation that can be solved by an iterative method to give the

altitude  $z$ . The first term on the right of equation 10 becomes

$$\ln \frac{p(z)}{p(90)} = - \frac{g_o M_o a^2}{T_m(90)R} \frac{z-90}{(a+z)(a+90)} \quad (11)$$

The second term becomes

$$\begin{aligned} \ln \frac{p(110)}{p(z)} = & - \frac{g_o M_o a^2}{[T_m(90) - (L)(a+90)]^2 R} \left\{ \frac{[T_m(90) - (L)(a+90)](z-90)}{(a+z)(a+90)} \right. \\ & \left. + L \ln \left[ \frac{a+90}{a+z} \frac{T_m(90) + (L)(z-90)}{T_m(90)} \right] \right\} \quad (12) \end{aligned}$$

The values  $p(90)$  and  $g_o$  are known from reference 2; the values  $p(110)$ ,  $a$ ,  $R$ , and  $T_m(110)$  from reference 1; and  $T_m(90)$  from the calculation. Since  $L$  is a function of  $z$

$$L = \frac{T_m(110) - T_m(90)}{110 - z} \quad (13)$$

equation 10 can be solved by iteration to find  $z$ .

After finding the altitude  $z$ , and  $p(z)$  by equation 11, we resumed the calculation of molecular scale temperatures and gradients for the altitude groups from 90 to 700 km, using the method outlined in section II-2.

Similar differences between references 3 and 1 exist at 90 km for the subarctic atmosphere. However, it was possible to generate a hydrostatically stable model without resorting to an artificial transition region. Research on the subarctic model will continue to determine whether such a region will indeed improve it. In any case, the present subarctic model is adequate for our purposes.

### SECTION III

#### APPLICATIONS

When fitting an atmosphere into a mesh of cells for the purpose of solving the hydrodynamic equations numerically on a computer, it is necessary to define a density and specific internal energy as well as a pressure to the atmosphere contained in each cell. Therefore, for a given altitude  $z$

$$p(z) = p(z_1)e^{-f} \quad (14)$$

where

$$f = \frac{g_0 M_0 a^2}{\left[ T_m(z_1) - (L_1)(a+z_1) \right]^2 R} \left\{ \frac{\left[ T_m(z_1) - (L_1)(a+z_1) \right] (z-z_1)}{(a+z)(a+z_1)} + L_1 \ln \left[ \frac{a+z_1}{a+z} \frac{T_m(z_1) + (L_1)(z-z_1)}{T_m(z_1)} \right] \right\} \quad (15)$$

and

$$z_1 \leq z < z_{i+1}$$

By the ideal gas law, the density at altitude  $z$  is

$$\rho(z) = \frac{p(z)}{p(o)} \frac{T_m(o)}{T_m(z)} \rho(o) \quad (16)$$

where  $p(o)$ ,  $\rho(o)$ , and  $T_m(o)$  are the sea level values for pressure, density, and molecular scale temperature, respectively.

To obtain the specific internal energy,  $i(z)$ , we require the equation of state for air which will be used in the calculation (e.g., the Doan-Nickel Equation of State for Air, reference 4) to return the same pressure as the



atmospheric model. This involves a solution by iteration which proceeds as follows. Guess a value for  $\gamma$ . Then, by the ideal gas law,

$$I(z) = \frac{p(z)}{(\gamma-1)\rho(z)} \quad (17)$$

where  $p(z)$  and  $\rho(z)$  are the values of pressure and density at altitude,  $z$ , as defined by the atmospheric model. Then these values for  $I(z)$  and  $\rho(z)$  are entered into the equation of state for air which returns a value for  $(\gamma_{\text{effective}} - 1)$ . Then, by the ideal gas law, the pressure is

$$p(z) = (\gamma_{\text{effective}} - 1)\rho(z)I(z) \quad (18)$$

The iteration continues until that combination of  $\gamma$  and  $I(z)$  is found, which will make the equation of state deliver the same pressure as the atmospheric model. See appendix.

## SECTION IV

## RESULTS

The annual mean temperate atmospheric model, the annual mean tropical atmospheric model, and the summer subarctic atmospheric model are given in tables II, III, and IV, respectively. Tables V, VI, and VII show the difference between the molecular scale temperatures at the base altitude of each altitude group as listed in references 1, 2, and 3 and those calculated for the atmospheric models.

The value for the altitude,  $z$ , used in the transition region of the tropical atmosphere is 97.84061 km; that is, the two altitude groups making up the transition region extend from 90 to 97.84061 km and from 97.84061 to 110 km.

The appendix contains the models in subroutine form.

Table II  
DEFINING PROPERTIES OF THE ANNUAL MEAN TEMPERATE ATMOSPHERE  
(45° N latitude)

Altitude z(cm)	Pressure (dynes/cm <sup>2</sup> )	Molecular scale temperature gradient L (°K/cm)	Molecular scale temperature T <sub>m</sub> (°K)
0.0000	1.01325 x 10 <sup>6</sup>	-6.49291767 x 10 <sup>-5</sup>	288.150000
1.1019 x 10 <sup>6</sup>	2.26320 x 10 <sup>5</sup>	9.28049177 x 10 <sup>-8</sup>	216.604540
2.0063 x 10 <sup>6</sup>	5.47487 x 10 <sup>4</sup>	9.86254816 x 10 <sup>-6</sup>	216.688473
3.2162 x 10 <sup>6</sup>	8.68014 x 10 <sup>3</sup>	2.77080370 x 10 <sup>-5</sup>	228.621170
4.7350 x 10 <sup>6</sup>	1.10905 x 10 <sup>3</sup>	-1.72246873 x 10 <sup>-7</sup>	270.704137
5.2429 x 10 <sup>6</sup>	5.90005 x 10 <sup>2</sup>	-1.95999298 x 10 <sup>-5</sup>	270.616652
6.1591 x 10 <sup>6</sup>	1.82099 x 10 <sup>2</sup>	-3.91697376 x 10 <sup>-5</sup>	252.659197
7.9994 x 10 <sup>6</sup>	1.03770 x 10 <sup>1</sup>	1.60823156 x 10 <sup>-7</sup>	180.575129
9.0000 x 10 <sup>6</sup>	1.64380 x 10 <sup>0</sup>	2.98166730 x 10 <sup>-5</sup>	180.736048
1.0000 x 10 <sup>7</sup>	3.0071 x 10 <sup>-1</sup>	5.02020153 x 10 <sup>-5</sup>	210.552722
1.1000 x 10 <sup>7</sup>	7.35440 x 10 <sup>-2</sup>	9.97762308 x 10 <sup>-5</sup>	260.754737
1.2000 x 10 <sup>7</sup>	2.52170 x 10 <sup>-2</sup>	2.00108806 x 10 <sup>-4</sup>	360.530968
1.5000 x 10 <sup>7</sup>	5.06170 x 10 <sup>-3</sup>	1.49589024 x 10 <sup>-4</sup>	960.857386
1.6000 x 10 <sup>7</sup>	3.69400 x 10 <sup>-3</sup>	1.00407491 x 10 <sup>-4</sup>	1110.446410
1.7000 x 10 <sup>7</sup>	2.79260 x 10 <sup>-3</sup>	6.97598503 x 10 <sup>-5</sup>	1210.853900
1.9000 x 10 <sup>7</sup>	1.68520 x 10 <sup>-3</sup>	5.01601097 x 10 <sup>-5</sup>	1350.373600
2.3000 x 10 <sup>7</sup>	6.96040 x 10 <sup>-4</sup>	3.98897144 x 10 <sup>-5</sup>	1551.014040
3.0000 x 10 <sup>7</sup>	1.88380 x 10 <sup>-4</sup>	3.31099390 x 10 <sup>-5</sup>	1870.242040
4.0000 x 10 <sup>7</sup>	4.03040 x 10 <sup>-5</sup>	2.58868496 x 10 <sup>-5</sup>	2161.341430
5.0000 x 10 <sup>7</sup>	1.09570 x 10 <sup>-5</sup>	1.71252931 x 10 <sup>-5</sup>	2420.209930
6.0000 x 10 <sup>7</sup>	3.45020 x 10 <sup>-6</sup>	1.09162418 x 10 <sup>-5</sup>	2591.462860
7.0000 x 10 <sup>7</sup>	1.19180 x 10 <sup>-6</sup>	...	2700.625280

$$a = 0.35670 \times 10^8 \text{ cm}$$

$$g = 9.80665 \times 10^2 \text{ cm/sec}^2$$

$$R = 8.31440 \times 10^7 \text{ erg/mole/deg K.}$$

$$M = 2.89644 \times 10^1 \text{ gm/mole}$$

Table III  
DEFINING PROPERTIES OF THE ANNUAL MEAN TROPICAL ATMOSPHERE  
(15° N latitude)

Altitude $z$ (cm)	Pressure (dynes/cm <sup>2</sup> )	Molecular scale temperature gradient $L$ (°K/cm)	Molecular scale temperature $T_m$ (°K)
0.000000	$1.013250 \times 10^6$	$-3.69962272 \times 10^{-5}$	299.650000
$2.254000 \times 10^5$	$7.813300 \times 10^5$	$-1.29419605 \times 10^{-4}$	291.311050
$2.505000 \times 10^5$	$7.586100 \times 10^5$	$-6.75109163 \times 10^{-5}$	288.062618
$1.657000 \times 10^6$	$1.013700 \times 10^5$	$4.11001824 \times 10^{-5}$	193.108515
$2.211300 \times 10^6$	$4.043000 \times 10^4$	$2.14811736 \times 10^{-5}$	215.890346
$4.743200 \times 10^6$	$1.188600 \times 10^3$	$4.20150001 \times 10^{-7}$	270.278529
$5.149800 \times 10^6$	$7.175600 \times 10^2$	$-1.93134924 \times 10^{-5}$	270.449362
$5.965200 \times 10^6$	$2.535100 \times 10^2$	$-3.43722620 \times 10^{-5}$	254.701140
$8.013000 \times 10^6$	$1.100100 \times 10^1$	$1.98418410 \times 10^{-7}$	184.313581
$9.000000 \times 10^6$	$1.862000 \times 10^0$	$-9.16634469 \times 10^{-7}$	184.509420
$9.784061 \times 10^6$	$4.549471 \times 10^{-1}$	$6.35832871 \times 10^{-5}$	183.790723
$1.100000 \times 10^7$	$7.354400 \times 10^{-2}$	$9.74012527 \times 10^{-5}$	261.104121
$1.200000 \times 10^7$	$2.521700 \times 10^{-2}$	$2.00803436 \times 10^{-4}$	358.505374
$1.500000 \times 10^7$	$5.061700 \times 10^{-3}$	$1.44417115 \times 10^{-4}$	960.915680
$1.600000 \times 10^7$	$3.694300 \times 10^{-3}$	$1.05385251 \times 10^{-4}$	1105.332790
$1.700000 \times 10^7$	$2.792600 \times 10^{-3}$	$6.68110562 \times 10^{-5}$	1210.718050
$1.900000 \times 10^7$	$1.685200 \times 10^{-3}$	$5.15616802 \times 10^{-5}$	1344.340160
$2.300000 \times 10^7$	$6.960400 \times 10^{-4}$	$3.88307486 \times 10^{-5}$	1550.586880
$3.000000 \times 10^7$	$1.883800 \times 10^{-4}$	$3.37947184 \times 10^{-5}$	1822.402120
$4.000000 \times 10^7$	$4.030400 \times 10^{-5}$	$2.49828094 \times 10^{-5}$	2160.349300
$5.000000 \times 10^7$	$1.095700 \times 10^{-5}$	$1.79900870 \times 10^{-5}$	2410.177400
$6.000000 \times 10^7$	$3.450200 \times 10^{-6}$	$9.94365149 \times 10^{-6}$	2590.078270
$7.000000 \times 10^7$	$1.191800 \times 10^{-6}$	...	2689.514780

$$a = 6.35670 \times 10^8 \text{ cm}$$

$$g_0 = 9.78381 \times 10^2 \text{ cm/sec}^2$$

$$R = 8.31440 \times 10^7 \text{ erg/mole/deg K.}$$

$$M = 2.99644 \times 10^1 \text{ gm/mole}$$

Table IV  
DEFINING PROPERTIES OF THE SUMMER SUBARCTIC ATMOSPHERE  
(60° N latitude)

Altitude $z$ (cm)	Pressure (dynes/cm <sup>2</sup> )	Molecular scale temperature gradient $L$ (°K/cm)	Molecular scale temperature $T_m$ (°K)
0.0000	$1.0100 \times 10^6$	$-5.15226593 \times 10^{-5}$	287.150000
$4.9980 \times 10^5$	$5.4154 \times 10^5$	$-7.45507917 \times 10^{-5}$	261.398975
$1.0003 \times 10^6$	$2.6758 \times 10^5$	$1.75752872 \times 10^{-6}$	224.086304
$2.3054 \times 10^6$	$3.7248 \times 10^4$	$1.21402825 \times 10^{-5}$	226.380054
$3.2121 \times 10^6$	$9.8883 \times 10^3$	$3.20422887 \times 10^{-5}$	237.387649
$4.3237 \times 10^6$	$2.2624 \times 10^3$	$5.54484005 \times 10^{-6}$	273.005857
$4.8303 \times 10^6$	$1.2140 \times 10^3$	$5.03741727 \times 10^{-6}$	275.814873
$5.3376 \times 10^6$	$6.5545 \times 10^2$	$-2.35321674 \times 10^{-5}$	278.370354
$5.9476 \times 10^6$	$3.0773 \times 10^2$	$-4.51273514 \times 10^{-5}$	264.015732
$7.9890 \times 10^6$	$1.2772 \times 10^1$	$-1.48868732 \times 10^{-6}$	171.892757
$9.0000 \times 10^6$	$1.7851 \times 10^0$	$3.31280965 \times 10^{-5}$	170.387694
$1.0000 \times 10^7$	$3.0075 \times 10^{-1}$	$6.61955253 \times 10^{-5}$	703.515791
$1.1000 \times 10^7$	$7.3544 \times 10^{-2}$	$8.07805343 \times 10^{-5}$	269.711316
$1.2000 \times 10^7$	$2.5217 \times 10^{-2}$	$2.10740515 \times 10^{-4}$	350.491850
$1.5000 \times 10^7$	$5.0617 \times 10^{-3}$	$1.06709040 \times 10^{-4}$	982.713396
$1.6000 \times 10^7$	$3.6943 \times 10^{-3}$	$1.47081912 \times 10^{-4}$	1089.422440
$1.7000 \times 10^7$	$2.7926 \times 10^{-3}$	$4.49679987 \times 10^{-5}$	1236.504250
$1.9000 \times 10^7$	$1.6852 \times 10^{-3}$	$6.37859718 \times 10^{-5}$	1326.440340
$2.3000 \times 10^7$	$6.9604 \times 10^{-4}$	$3.13145277 \times 10^{-5}$	1581.584230
$3.0000 \times 10^7$	$1.8838 \times 10^{-4}$	$3.99574107 \times 10^{-5}$	1800.785930
$4.0000 \times 10^7$	$4.0304 \times 10^{-5}$	$1.82856612 \times 10^{-5}$	2200.360030
$5.0000 \times 10^7$	$1.0957 \times 10^{-5}$	$2.52271247 \times 10^{-6}$	2384.216670
$6.0000 \times 10^7$	$3.4502 \times 10^{-6}$	$2.47207416 \times 10^{-6}$	2636.487910
$7.0000 \times 10^7$	$1.1918 \times 10^{-6}$	---	2661.208650

$$a = 6.35670 \times 10^8 \text{ cm}$$

$$g_0 = 9.81911 \times 10^2 \text{ cm/sec}^2$$

$$R = 8.31440 \times 10^7 \text{ erg/mole/deg K}$$

$$M = 2.89644 \times 10^3 \text{ gm/mole}$$

Table V

DIFFERENCES BETWEEN CALCULATED AND TABULATED MOLECULAR  
SCALE TEMPERATURES IN THE TEMPERATE ATMOSPHERIC MODEL

Altitude (cm)	Tabulated temperatures (°K)	Calculated temperatures (°K)	% Difference
0.0000	288.15	288.15	0.000
$1.1019 \times 10^6$	216.65	216.60	-0.021
$2.0063 \times 10^6$	216.65	216.69	0.018
$3.2162 \times 10^6$	228.65	228.62	-0.013
$4.7350 \times 10^6$	270.65	270.70	0.020
$5.2429 \times 10^6$	270.65	270.62	-0.012
$6.1591 \times 10^6$	252.65	252.66	0.004
$7.9994 \times 10^6$	180.65	180.58	-0.041
$9.0000 \times 10^6$	180.65	180.74	0.048
$1.0000 \times 10^7$	210.65	210.55	-0.046
$1.1000 \times 10^7$	260.65	260.75	0.040
$1.2000 \times 10^7$	360.65	360.53	-0.033
$1.5000 \times 10^7$	960.65	960.86	0.022
$1.6000 \times 10^7$	1110.65	1110.45	-0.018
$1.7000 \times 10^7$	1210.65	1210.85	0.017
$1.9000 \times 10^7$	1350.65	1350.37	-0.020
$2.3000 \times 10^7$	1550.65	1551.01	0.023
$3.0000 \times 10^7$	1830.65	1830.24	-0.022
$4.0000 \times 10^7$	2160.65	2161.34	0.032
$5.0000 \times 10^7$	2420.65	2420.71	0.001
$6.0000 \times 10^7$	2590.65	2591.46	0.031
$7.0000 \times 10^7$	2700.65	2700.63	-0.001

Table VI

DIFFERENCES BETWEEN CALCULATED AND TABULATED MOLECULAR  
SCALE TEMPERATURES IN THE TROPICAL ATMOSPHERIC MODEL

Altitude (cm)	Tabulated temperatures (°K)	Calculated temperatures (°K)	% Difference
0.000000	299.65	299.65	0.000
2.254000 x 10 <sup>5</sup>	286.15	291.31	1.204
2.505000 x 10 <sup>5</sup>	286.95	288.06	0.388
1.657000 x 10 <sup>6</sup>	193.15	193.11	-0.021
2.211000 x 10 <sup>6</sup>	215.15	215.89	0.344
4.743200 x 10 <sup>6</sup>	270.15	270.28	0.048
5.198000 x 10 <sup>6</sup>	270.15	270.45	0.111
5.965200 x 10 <sup>6</sup>	254.15	254.70	0.217
8.013000 x 10 <sup>6</sup>	184.15	184.31	0.089
9.000000 x 10 <sup>6</sup>	184.15	184.51	0.925
9.784061 x 10 <sup>7</sup>	184.15	183.79	-0.191
1.100000 x 10 <sup>7</sup>	260.65	261.10	0.174
1.200000 x 10 <sup>7</sup>	360.65	358.51	-0.595
1.500000 x 10 <sup>7</sup>	960.65	960.72	0.028
1.600000 x 10 <sup>7</sup>	1110.65	1105.33	-0.478
1.700000 x 10 <sup>7</sup>	1210.65	1210.72	0.006
1.900000 x 10 <sup>7</sup>	1350.65	1344.34	-0.467
2.300000 x 10 <sup>7</sup>	1550.65	1550.59	-0.004
3.000000 x 10 <sup>7</sup>	1830.65	1822.40	-0.451
4.000000 x 10 <sup>7</sup>	2160.65	2160.35	-0.014
5.000000 x 10 <sup>7</sup>	2420.65	2419.18	-0.432
6.000000 x 10 <sup>7</sup>	2590.65	2590.08	-0.022
7.000000 x 10 <sup>7</sup>	2700.65	2689.51	-0.412

Table VII

DIFFERENCES BETWEEN CALCULATED AND TABULATED MOLECULAR  
SCALE TEMPERATURES IN THE SUPAC TIC ATMOSPHERIC MODEL

Altitude (cm)	Tabulated temperatures (°K)	Calculated temperatures (°K)	% Difference
0.0000	287.15	287.15	0.000
4.9980 x 10 <sup>5</sup>	260.15	261.40	0.480
1.0003 x 10 <sup>6</sup>	225.15	224.09	-0.472
2.3054 x 10 <sup>6</sup>	225.15	226.38	0.546
3.2121 x 10 <sup>6</sup>	238.65	237.39	-0.529
4.3237 x 10 <sup>6</sup>	271.65	273.00	0.499
4.8303 x 10 <sup>6</sup>	277.15	275.81	-0.482
5.3376 x 10 <sup>6</sup>	277.15	278.37	0.440
5.9476 x 10 <sup>6</sup>	265.15	264.02	-0.428
7.9890 x 10 <sup>6</sup>	171.15	171.90	0.434
9.0000 x 10 <sup>6</sup>	171.15	170.39	-0.445
1.0000 x 10 <sup>7</sup>	210.65	203.52	-3.387
1.1000 x 10 <sup>7</sup>	260.65	269.71	3.476
1.2000 x 10 <sup>7</sup>	360.65	350.49	-2.817
1.5000 x 10 <sup>7</sup>	960.65	962.71	2.297
1.6000 x 10 <sup>7</sup>	1110.65	1089.42	-1.911
1.7000 x 10 <sup>7</sup>	1210.65	1236.50	2.136
1.9000 x 10 <sup>7</sup>	1350.65	1326.44	-1.792
2.3000 x 10 <sup>7</sup>	1550.65	1581.58	1.990
3.0000 x 10 <sup>7</sup>	1830.65	1800.79	-1.631
4.0000 x 10 <sup>7</sup>	2160.65	2200.36	1.837
5.0000 x 10 <sup>7</sup>	2420.65	2384.22	-1.505
6.0000 x 10 <sup>7</sup>	2590.65	2636.49	1.769
7.0000 x 10 <sup>7</sup>	2700.65	2661.21	-1.460



## SECTION V

## CONCLUSIONS

The atmospheric models are derived such that the hydrostatic equation is satisfied.

$$\frac{d[p(z)]}{dz} = -\rho(z)g(z)$$

In general, hydrodynamic computer codes calculate  $dp/dz$ , the pressure gradient, by finite difference methods which replace  $dp/dz$  by  $\Delta p/\Delta z$ . This approximation results in unwanted accelerations which can be written as

$$a = \frac{\left(\frac{dp}{dz}\right)_z - \left(\frac{\Delta p}{\Delta z}\right)_z}{\rho(z)}$$

For example, given a code in which

$$\left(\frac{\Delta p}{\Delta z}\right)_z = \frac{p(z+\Delta z) - p(z-\Delta z)}{2\Delta z}$$

and assuming a scale height,  $H$ , constant over the interval,  $\Delta z$ , so that the pressure,  $p(z)$ , can be written

$$p(z) = p(z_0)e^{-\frac{z-z_0}{H}}$$

one can expand  $(\Delta p/\Delta z)$  in powers of  $\Delta z/H$  so that to second order, the net accelerations are

$$a = \frac{1}{6} g(z) \left(\frac{\Delta z}{H}\right)^2$$

For all practical purposes, this acceleration is negligible until the zone size,  $\Delta z$ , becomes greater than a tenth of a kilometer. For example, at an altitude of 250 km, the scale height,  $H$ , is about 5 kilometers and  $g$  about  $900 \text{ cm/sec}^2$ . At 250 km, the scale height has its smallest value in the atmosphere so this example will give a measure of the worst acceleration. If  $\Delta z$  is 0.1 km, the above relationship gives an acceleration of  $0.05 \text{ cm/sec}^2$ . If  $\Delta z$  is 1 km, the acceleration is  $5.0 \text{ cm/sec}^2$ .

The pressures and densities given by the atmospheric models agree with tabulated values in references 1 and 2 to one part in  $10^6$  and temperatures to one part in 100.

# APPENDIX

## SUBROUTINE ATMOS

The FORTRAN subroutine appearing in this appendix is the annual mean temperate atmospheric model. By inputting an altitude, TTY, the subroutine will return

WSP	the pressure at that altitude
WSR	the density at that altitude
WST	the temperature at that altitude
WSI	the specific internal energy at that altitude
WSU	the radial velocity = 0
WSV	the axial velocity = 0
GMONE	$\gamma - 1$ .

For the annual mean tropical atmospheric model or the summer subarctic atmospheric model, replace the data in the TABZ, TABL, TABT, and TABP blocks with the data appearing in tables III or IV as appropriate.

```

SUBROUTINE ATMOSPHERE(WSP,WSR,WST,WSI,WSU,WSV,GMONE)
  DIMENSION TABZ(22), TABL(22), TART(22), TARP(22)

```

```

      CALCULATE ATMOSPHERE

```

```

      A=RADIUS OF THE EARTH IN CM.
      G=ACCELERATION DUE TO GRAVITY IN CM./SEC./SEC.
      =980.465 FOR THE TEMPERATE ATMOSPHERE
      =978.381 FOR THE TROPICAL ATMOSPHERE
      =981.011 FOR THE SUBARCTIC ATMOSPHERE
      R=GAS CONSTANT IN ERGS/MOLE/DEG.
      W=MOLECULAR WEIGHT OF AIR

```

```

      A=6.3567E+08
      G=9.80665E+02
      R=8.3144E+07
      W=2.89644E+01

```

```

      THE FOLLOWING DATA IN TABZ, TABL, TART, AND TARP ARE FROM TABLE 2
      FOR THE TEMPERATE ATMOSPHERE. FOR THE TROPICAL OR SUBARCTIC ATMOS-
      PHERES SUBSTITUTE THE DATA FROM TABLES 3 AND 4 RESPECTIVELY.

```

```

      TABZ IS THE BASE ALTITUDE OF EACH ALTITUDE GROUP IN CM.

```

```

      TABZ( 1)=0.
      TABZ( 2)=1.1010E+04
      TABZ( 3)=2.0063E+06
      TABZ( 4)=3.2162E+06
      TABZ( 5)=4.7350E+06
      TABZ( 6)=5.2429E+06
      TABZ( 7)=6.1591E+06
      TABZ( 8)=7.9994E+06
      TABZ( 9)=9.0E+06
      TABZ(10)=10.0E+06
      TABZ(11)=11.0E+06
      TABZ(12)=12.0E+06
      TABZ(13)=15.0E+06
      TABZ(14)=16.0E+06
      TABZ(15)=17.0E+06
      TABZ(16)=19.0E+06
      TABZ(17)=23.0E+06
      TABZ(18)=30.0E+06
      TABZ(19)=40.0E+06
      TABZ(20)=50.0E+06
      TABZ(21)=60.0E+06
      TABZ(22)=70.0E+06

```

```

      TABL IS THE MOLECULAR SCALE TEMPERATURE GRADIENT OF EACH ALTITUDE
      GROUP IN DEG./CM.

```

```

      TABL( 1)=-6.49291767E-05
      TABL( 2)= 9.28049177E-08
      TABL( 3)= 9.86254816E-06
      TABL( 4)= 2.77080370E-05
      TABL( 5)=-1.72246873E-07
      TABL( 6)=-1.25092298E-05
      TABL( 7)=-2.01697776E-05
      TABL( 8)= 1.60823156E-07

```

Best Available Copy

TABL( 9)= 2.98166708E-05  
 TABL(10)= 5.02020153E-05  
 TABL(11)= 9.97762308E-05  
 TABL(12)= 2.00108806E-04  
 TABL(13)= 1.49589024E-04  
 TABL(14)= 1.00407491E-04  
 TABL(15)= 6.07598503E-05  
 TABL(16)= 5.01601097E-05  
 TABL(17)= 3.08927144E-05  
 TABL(18)= 3.31099390E-05  
 TABL(19)= 2.58358496E-05  
 TABL(20)= 1.71252931E-05  
 TABL(21)= 1.09162418E-05

C TABT IS THE MOLECULAR SCALE TEMPERATURE CORRESPONDING TO THE TABZ  
 IN DEGREES KELVIN

TART( 1)= 2.88150000E+02  
 TART( 2)= 2.16604540E+02  
 TART( 3)= 2.16688473E+02  
 TART( 4)= 2.28621170E+02  
 TART( 5)= 2.70704137E+02  
 TART( 6)= 2.70616652E+02  
 TART( 7)= 2.52659197E+02  
 TART( 8)= 1.80575129E+02  
 TART( 9)= 1.90736048E+02  
 TART(10)= 2.10552722E+02  
 TART(11)= 2.60754737E+02  
 TART(12)= 3.60530968E+02  
 TART(13)= 9.60857386E+02  
 TART(14)= 1.11044641E+03  
 TART(15)= 1.21085390E+03  
 TART(16)= 1.35037360E+03  
 TART(17)= 1.55101404E+03  
 TART(18)= 1.83024204E+03  
 TART(19)= 2.16134143E+03  
 TART(20)= 2.42020993E+03  
 TART(21)= 2.59146286E+03  
 TART(22)= 2.70062528E+03

C TARP IS THE PRESSURE CORRESPONDING TO THE TABZ IN DYNES/CM./CM.

TARP( 1)=1.01325E+06  
 TARP( 2)=2.26320E+05  
 TARP( 3)=5.47487E+04  
 TARP( 4)=8.68014E+03  
 TARP( 5)=1.10905E+03  
 TARP( 6)=5.90005E+02  
 TARP( 7)=1.82099E+02  
 TARP( 8)=1.0377E+01  
 TARP( 9)=1.5438E+00  
 TARP(10)=3.0075E-01  
 TARP(11)=7.3544E-02  
 TARP(12)=2.5217E-02  
 TARP(13)=5.0617E-03  
 TARP(14)=3.6943E-03  
 TARP(15)=2.7926E-03  
 TARP(16)=1.6852E-03  
 TARP(17)=6.9604E-04

Best Available Copy

```

TARP(18)=1.8838E-04
TARP(19)=4.0304E-05
TARP(20)=1.0957E-05
TARP(21)=3.4502E-06
TARP(22)=1.1918E-06

C
RHOZ=W*TARP(1)/(TART(1)*R)
EZ=1.F+10

C
DO 80 JAT=1,21    FOR THE TEMPERATE ATMOSPHERE
C
DO 80 JAT=1,22    FOR THE TROPICAL ATMOSPHERE
C
DO 80 JAT=1,23    FOR THE SUBARCTIC ATMOSPHERE
C

DO 80 JAT=1,21
IF(TTY-TABZ(JAT))81,82,80
80 CONTINUE
C
JAT=21 FOR THE TEMPERATE ATMOSPHERE
C
JAT=22 FOR THE TROPICAL ATMOSPHERE
C
JAT=23 FOR THE SUBARCTIC ATMOSPHERE
JAT=21
GO TO 82
81 JAT=JAT-1
82 CONS=A*A*G*W/R
DUM2=(TTY-TABZ(JAT))/((A+TTY)*(A+TABZ(JAT)))
DUM3=(A+TABZ(JAT))/(A+TTY)
VAR1=TART(JAT)-TABL(JAT)*(A+TABZ(JAT))
VAR2=(TABT(JAT)+TABL(JAT)*(TTY-TABZ(JAT)))/TART(JAT)
FS=CONS/(VAR1*VAR1)*((VAR1*DUM2+TABL(JAT)*LOGF(DUM3*VAR2))
WSP=TARP(JAT)*EXP(-FS)
WST=TART(JAT)+TABL(JAT)*(TTY-TABZ(JAT))
WSR=WSP*TART(1)*RHOZ / (WST*TARP(1))

C
C CALCULATE THE INTERNAL ENERGY
C
FSO=0.
GAM1=.5
DGM=-0.001
880 RHO=WCD
E=WSP/(GAM1*WSP)
ENY=F

C
C DOAN-NICKEL SEMI-PHYSICAL FIT TO THE EQUATION OF STATE OF AIR
C
C TEMPERATURES FROM .025 TO 1.5 ELECTRON VOLTS
C DENSITIES FROM 10**2 TO 10**(-7) NORMAL DENSITY
C PRESSURE = (GAMMA-1.)*RHO*E, WHERE GAMMA IS A FUNCTION OF
C DENSITY AND ENERGY
C RHO = MATERIAL DENSITY
C RHO7 = 1.2936 MEGAGRAMS/CUBIC KILOMETER, IN THE UNITS OF THE
C PROBLEM
C E = ENERGY/MASS
C EZ = 1 JERK/MEGAGRAM, IN THE UNITS OF THE PROBLEM
C GMONE = GAMMA MINUS ONE
C MAKE F POSITIVE IF NEGATIVE, AND CONVERT TO JERKS/MEGAGRAM
102 E=ABS(F)/EZ

```

```

POWER=-ALOG(RHO/RHOZ)/2.3025851
~ THE ENERGY AT WHICH OXYGEN AND NITROGEN DISSOCIATE IS A
C FUNCTION OF DENSITY
E1=(8.5-E)/.975
C THE FERMI-DIRAC FUNCTION IS ONLY COMPUTED WITHIN 5.*DELTA E OF
C EACH TRANSITION. OTHERWISE IT IS ONE OR ZERO
IF (AMSE(E1)-5.) 106,103,103
103 IF (E1) 105,105,104
104 FO=EXP(-E/4.46)
FON=0.
WS=1.
GO TO 107
105 FO=0.
FON=EXP(-E/6.63)
WS=0.
GO TO 107
106 DE1=.075*(RHO/RHOZ)**.05
EE1=8.5-.357*POWER
E1=(EE1-E)/DE1
WS=1./(EXP(-E1)+1.)
FO=EXP(-E/4.46)*WS
FON=EXP(-E/6.63)*(1.-WS)
C THE DENSITY DEPENDENCE ONLY OCCURS ABOVE E=1., AND IT IS OF
C THE FORM (RHO/RHOZ)**(CONSTANT*LOG(E)). THE CONSTANT
C MAKES A TRANSITION FROM .048 TO .029 AS THE OXYGEN DISSOCIATES
C AND THE DENSITY SPREAD BECOMES CONSTANT BEYOND THE THIRD PEAK
107 IF (E-1.) 108,108,109
108 BETA=0.
GO TO 110
109 BETA=(.048*WS+.032*(1.-WS))*ALOG(E)/2.3025851
110 E2=(E-40.)/3.
IF (AMSE(E2)-5.) 114,111,111
111 IF (E2) 112,112,113
112 FN=0.
WS=0.
GO TO 115
113 FN=EXP(-E/25.5)
WS=1.
GO TO 115
114 DE2=4.*(RHO/RHOZ)**.085
EE2=45.*(RHO/RHOZ)**.0157
E2=(E-EE2)/DE2
WS=1./(EXP(-E2)+1.)
FN=EXP(-E/25.5)*WS
115 E3=(E-160.)/6.
BETA=BETA*(1.-WS)+.045*WS
IF (E3+E.) 116,117,117
116 FE=0.
GO TO 118
117 FE=1./(EXP(-E3)+1.)
118 RHOEFAC=(RHO/RHOZ)**BETA
GMONE=(.161+.255*FO+.280*FON+.137*FN+.050*FE)*RHOEFAC
P=GMONE*ENY*RHO
FS=P-UCD
IF (FS) 009,1004,009

```

```

099  IF(FS=FS0)1001,1000,1000
1000  GAM1=GAM1+DGM
      FS0=FS
      GO TO 1002
1001  GAM1=GAM1-DGM
      DGM=DGM/100.
      GAM1=GAM1+DGM
1002  IF(GAM1)1004,1003,1003
1003  IF(ABSF(DGM)-1.0E-10)1004,900,900
1004  WSI= P/(GMONE*WSR)
      WSU=0.
      WSV=0.
      RETURN
      END

```



#### REFERENCES

1. US Standard Atmosphere-1962, US Government Printing Office, Washington, DC, 1962.
2. Court, A., A. J. Kantor, A. E. Cole, Supplemental Atmospheres, AFCRL-62-899, Air Force Cambridge Research Laboratories, L. G. Hanscom Field, Massachusetts, September 1962.
3. Cole, A. E., A. J. Kantor, Air Force Interim Supplemental Atmospheres to 90 Kilometers, AFCRL-63-936, Air Force Cambridge Research Laboratories, L. G. Hanscom Field, Massachusetts, December 1962.
4. Doan, L. R., G. H. Nickel, A Subroutine for the Equation of State of Air, RTD (WLR) TM-63-2, Air Force Weapons Laboratory, Kirtland AFB, New Mexico, May 1963.

DISTRIBUTION

No. CYS

HEADQUARTERS USAF

Hq USAF, Wash, DC 20330

- 1 (AFWIN)
- 1 (AFTAC)
- 1 (AFTAC/TD-3, Capt Herman)
- 1 (AFRSTG)
- 1 USAF Dep, The Inspector General (AFIDI), Norton AFB, Calif 92409
- 1 USAF Directorate of Nuclear Safety (AFINS), Kirtland AFB, NM 87117

MAJOR AIR COMMANDS

AFSC, Andrews AFB, Wash, DC 20331

- 1 (SCTSE)
- 1 (SCTSW)
- 1 (SCTLI)
- 1 TAC (DORQ-M), Langley AFB, Va 23365
- SAC, Offutt AFB, Nebr 68113
- 1 (OA)
- 1 (BME)
- 1 AFLC (MCPTH), Wright-Patterson AFB, Ohio 45433
- 1 ADC (ADOOA), Ent AFB, Colo 80912
- 1 AUL Maxwell AFB, Ala 36112
- USAF, Colo 80840
- 1 (DFLBA)
- 1 (Comad Nike-X Impact Task Force, ATTN: Capt John Ahearne, THL DFA, Sgt George)

AFSC ORGANIZATIONS

- 1 AFSC Scientific and Technical Liaison Office, Research and Technology Division, AFMDO, Los Angeles, Calif 90045
- 1 AFSC Scientific and Technical Liaison Office (RTSAS), Suite 104, 363 South Tasffe Ave, Sunnyvale, Calif 94086
- 1 FTD (TDHIL), Wright-Patterson AFB, Ohio 45433
- 1 AF Materials Laboratory, Wright-Patterson AFB, Ohio 45433
- 1 AF Avionics Laboratory, Wright-Patterson AFB, Ohio 45433
- 1 AF Flight Dynamics Laboratory, Wright-Patterson AFB, Ohio 45433
- 1 AF Aero-Propulsion Laboratory, Wright-Patterson AFB, Ohio 45433
- 1 SEC (SEFIR), Wright-Patterson AFB, Ohio 45433
- 1 OLA (RRRD), Holloman AFB, NM 88330

DISTRIBUTION (cont'd)

No. cys

1 AEDC (AEYD), Arnold AFS, Tenn 37289  
 1 ESD (ESTI), L. G. Hanscom Fld, Bedford, Mass 01731  
 1 Air Force Cambridge Research Laboratories, ATTN: Dr. K. Champion,  
 L. G. Hanscom Fld, Bedford, Mass 01731  
 2 SAMSO (SMY), AFUPO, Los Angeles, Calif 90045  
 1 APGC (PGBPS-12), Eglin AFB, Fla 32542  
 1 RADC (EMLAL-1), Griffiss AFB, NY 13442

KIRTLAND AFB ORGANIZATIONS

1 AFSWC (SWEH), Kirtland AFB, NM 87117  
 1 ADC (ADSWC), Special Weapons Office, Kirtland AFB, NM 87117  
 1 SAC Res Rep (SACLO), AFSWC, Kirtland AFB, NM 87117  
 1 TAC Liaison Office (TACLO-s), AFSWC, Kirtland AFB, NM 87117  
 AFWL, Kirtland AFB, NM 87117  
 12 (WIL)  
 1 (WLAA)  
 1 (WLAW)  
 1 (WLDC, Lt H. Cooper)  
 1 (WLOM)  
 1 (WLRE)  
 1 (WLRE)  
 1 (WLRP)  
 20 (WLRI)  
 1 (WLX)

OTHER AIR FORCE AGENCIES

Director, USAF Project RAND, via: AFLO, The RAND Corporation,  
 1700 Main Street, Santa Monica, Calif 90406

1 (RAND Physics Div)  
 1 (RAND Library)  
 1 Hq OAR (RROS), 1400 Wilson Blvd, Arlington, Va 22209  
 1 AFOSR, 1400 Wilson Blvd, Arlington, Va 22209

ARMY ACTIVITIES

1 Chief of Research and Development, Department of the Army (CRD/P,  
 Scientific and Technical Information Division), Wash, DC 20310  
 1 Commanding Officer, Harry Diamond Laboratories, ATTN: Library,  
 Wash, DC 20438  
 1 JS Army Materiel Command, NIKE-X Fld Ofc (AMCPM-NXE-FB, Lt Col F. G.  
 Thomas), Bell Telephone Laboratories, Inc., Shippany, NJ 07981

DISTRIBUTION (cont'd)

No. cys

- 1 Redstone Scientific Information Center, US Army Missile Command,  
Chief, Document Section, Redstone Arsenal, Ala 35809  
Commanding Officer, Ballistic Research Laboratories, Aberdeen  
Proving Ground, Md 21005
- 1 (AMXBR-TB, Mr. J. Meszaros)
- 1 (AMXBR)
- 1 (Mr. J. R. Kelso)
- 1 (Mr. R. Reisler)
- 1 (Mr. J. Keefer)
- 1 (AFLO)
- 1 Director, Army Research Office, 3045 Columbia Pike, Arlington, Va  
22204  
Director, US Army Waterways Experiment Sta (WESRL), P. O. Box 631,  
Vicksburg, Miss 39181
- 1 (Mr. A. D. Rooke)
- 1 (Mr. D. W. Murrel)
- 1 (A. L. Matthews)
- 2 Director, US Army Engineer Research and Development Laboratories,  
ATTN: STINFO Branch, Ft Belvoir, Va 20260
- 1 Commanding General, White Sands Missile Range (Tech Lib), White  
Sands, NM 88002
- 1 Commanding Officer (SMUPA-VCI, Samuel Feltman Research Laboratories),  
Picatinny Arsenal, Dover, NJ 07801

NAVY ACTIVITIES

- 1 Chief of Naval Research, Department of the Navy, Wash, DC 20390
- 1 Naval Air Systems Command (Code AIR-52023), Department of the Navy,  
Wash, DC 20360
- 1 Commanding Officer, Naval Research Laboratory, Wash, DC 20390
- 1 Commanding Officer and Director, US Naval Radiological Defense  
Laboratory, San Francisco, Calif 94135
- 1 Commanding Officer and Director, Naval Ship Research and Development  
Center, Wash, DC 20007
- 1 Superintendent, US Naval Postgraduate School, ATTN: G. R. Luckett,  
Monterey, Calif 93940
- 1 Commanding Officer and Director, Naval Civil Engineering Laboratory,  
Port Hueneme, Calif 93041
- 1 Commanding Officer and Director, Naval Applied Science Laboratory,  
Brooklyn, NY 11251
- 1 Commander, Naval Ordnance Test Station (Code 753), China Lake,  
Calif 93557

## DISTRIBUTION (cont'd)

No. cys

- 2 Commander, Naval Ordnance Laboratory, ATTN: Dr. Rudlin, White Oak, Silver Spring, Md 20910
- 1 Officer-in-Charge, Naval Civil Engineering Corps Officers School, US Naval Construction Battalion Center, Port Hueneme, Calif 93041
- 1 Director of Naval Warfare Analyses, Institute of Naval Studies, Office of the Chief of Navy Ops, 545 Technology Square, Cambridge, Mass 02139
- 1 Commanding Officer, NWEF (Code WE), Kirtland AFB, NM 87117

## OTHER DOD ACTIVITIES

- Director, DASA, Wash, DC 20305
- 2 (Document Library Branch)
- 1 (Mr. Mort Rubenstein)
- 1 (Maj. Choromokos)
- 1 (Col Brown)
- 1 (Dr. Wikner)
- 1 Commander, Fld Cmd, DASA (FCAG3, Spec Wpns Pub Dist), Sandia Base, NM 87115
- Office of Director of Defense Research and Engineering, Office of Atomic Programs, Rm 3E1071, The Pentagon, Wash, DC 20330
- 1 (John E. Jackson)
- 1 (Brig Gen Glen Kent)
- 1 Director, Advanced Research Projects Agency, DOD, Pentagon, Wash, DC 20301
- 20 DDC (TIAAS), Cameron Station, Alexandria, Va 22314

## AEC ACTIVITIES

- 1 USAEC (Hq Lib, Rpts Sect), Mail Sta G-017, Wash, DC 20454
- Sandia Corporation, Box 5800, Sandia Base, NM 87115
- 2 (Info Dist Div)
- 1 (Mr. Richard Bass)
- 1 (Mr. D. R. Breeding)
- 2 Sandia Corp (Tech Lib), P. O. Box 969, Livermore, Calif 94551
- 1 Chief, Div Tech Info Ext, USAEC, Box 62, Oak Ridge, Tenn 37831
- 1 UCLRL, ATTN: Dr. W. G. Magnuson, Jr., P. O. Box 808, Livermore, Calif 94551
- 1 UCLRL (Tech Info Div), Berkeley, Calif 94720
- 2 Director, LASL (H. Redman, Rpt Lib), P. O. Box 1663, Los Alamos, NM 87554
- 1 Courant Inst Math Sci, AECCAMC (Tech Lib), 251 Mercer St. New York, NY 10012

## DISTRIBUTION (cont'd)

No. cya

## OTHER

- 1 Langley Research Cen (NASA), Assoc Dir, Langley Sta, Hampton, Va 23365
- 1 Manned Spacecraft Cen (NASA), Ch, Tech Info Div, Houston, Tex 77001
- 1 Institute for Defense Analysis, Rm 2B257, Pentagon, Wash, DC 20330  
THRU: ARPA
- 1 Research Analysis Corp (M. L. Emerson, Lib), McLean, Va 22101  
MIT, Lincoln Laboratory, P. O. Box 73, Lexington, Mass 02173
- 1 (Document Library)
- 1 (Aeroelastic Structures Lab, Mr. Frank Durgan)
- 1 Aerospace Corp, P. O. Box 95085, Los Angeles, Calif 90045  
TRW Systems, Engineering Mechanics Laboratory, One Space Park,  
R 1/1004, Redondo Beach, Calif 90278
- 1 (Mr. F. B. Fay, Staff Engineer)
- 1 (Mr. Burt Peterson)
- 1 (F. Galbraith)
- 1 Aerospace Corp, ATTN: A. M. Naqvi, San Bernardino Operations,  
P. O. Box 1308, San Bernardino, Calif 92402
- 1 University of New Mexico, CERF, ATTN: Dr. Zwoyer, Box 188,  
University Station, Albuquerque, NM 87103
- 1 Applied Physics Laboratory, Johns Hopkins University, 8621 Georgia  
Aven, Silver Spring, Md 20910
- 1 AVCO Corp, RAD (Chief Librarian), 201 Lowell St, Wilmington, Mass  
01887
- 1 Forrestal Research Center Library, Aeronautical Sciences Bldg,  
Princeton University, Princeton, NJ 08540
- 1 General Atomic Division, General Dynamics Corp, P. O. Box 608,  
San Diego, Calif 92121  
General Electric Co, TEMPO, 816 State St, Santa Barbara, Calif 93101
- 1 (DASA Info and Anlys Cen)
- 1 (Mr. Bill Hart)
- 1 University of Illinois, ATTN: Dr. N. M. Newmark, Head, Civil  
Engineering Dept, 1114 Civil Engineering Bldg, Urbana, Ill 61801
- 1 College Park Metallurgy Center, US Bureau of Mines (Library),  
College Park, Md 20741
- 1 University of Massachusetts, Head, Civil Engineering Dept, Amherst,  
Mass 01002
- 1 University of Michigan, ATTN: Prof. R. G. Johnston, Dept of Civil  
Engineering, Ann Arbor, Mich 48104

## DISTRIBUTION (cont'd)

No. cys

Space Technology Laboratories, Inc., Bldg S/1930, One Space Park,  
Redondo Beach, Calif 90278

1 (AF Contr Mgt Ofc, c/o STLTD)

1 (Mr. F. A. Pieper)

Stanford Research Institute, Menlo Park, Calif 94025

1 (T. D. Witherly)

1 (Mr. C. Vincent)

1 (G-037, External Reports)

1 (Mr. E. Wood)

1 (Mr. B. Barclay)

1 The Boeing Company, ATTN: R. H. Carlson, 1707 First National Bank  
Bldg East, 5301 Central Ave NE, Albuquerque, NM 87108

1 Lockheed Missiles and Space Co, ATTN: Dr. R. E. Meyerott, 3251  
Hanover St, Palo Alto, Calif 94304

1 Kaman Nuclear, Div Kaman Acft Corp, ATTN: Dr. A. P. Bridges, Garden  
of the Gods Road, Colorado Springs, Colo 80907

Bell Telephone Laboratories, Inc, Whippany, NJ 07981

1 (J. W. Foss)

1 (Mr. William Troutman)

1 (Mr. T. Gressitt)

1 General American Transportation Co, Research Div, Mr. Milton R.  
Johnson, GATX, 7501 N. Natchez Ave, Niles, Ill 60648

Physics International Co, 2700 Merced St, San Leandro, Calif 94577

1 (Library)

1 (Dr. Charles S. Godfrey)

1 (Mr. Dean M. Christensen)

1 Bechtel Corp, Mr. William G. Bingham, Jr., 4550 Seville Ave, Vernon,  
Calif 90058

1 Holmes & Narver, Inc., Special Projects Div, Mr. S. B. Smith, 849  
South Broadway, Los Angeles, Calif 90014

1 United Research Services, 1811 Trousdale Dr, Burlingame, Calif 94010

1 Southwest Research Inst, Mr. M. L. Whitfield, 8500 Culebra Rd, San  
Antonio, Tex 78228

1 University of Michigan Inst of Sci & Tech, Mr. Gordon Frantti, P. O.  
Box 618, Ann Arbor, Mich 48104

1 Princeton University, Dr. Walker Bleakney, Palmer Physical Lab,  
Princeton, NJ 08540

1 MIT, Dr. Robert Hansen, 77 Massachusetts Ave, Cambridge, Mass 02139

DISTRIBUTION (cont'd)

No. cys

- 1 St Louis University, Dr. Carl Kisslinger, 221 N. Grand, St Louis, Mo 63100
- 1 IITRI, Dr. Eugene Sevin, 10 W. 35 St., Chicago, Ill 60616
- 1 University of Denver, John Wisotski, Denver Research Institute, Denver, Colo 80210
- 1 New Mexico Institute of Mining and Technology, Mr. M. Hanson, College Station, Socorro, NM 87801
- 1 Engineering Physics Co, William Danek, Jr, 12721 Twinbrook Parkway, Rockville, Md 20852
- 1 Official Record Copy (Lt Brackbill, WLRT)



UNCLASSIFIED  
Security Classification

DOCUMENT CONTROL DATA - R&D		
(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)		
1. ORIGINATING ACTIVITY (Corporate author) Air Force Weapons Laboratory (WLRT) Kirtland Air Force Base, New Mexico 87117		2a. REPORT SECURITY CLASSIFICATION UNCLASSIFIED
		2b. GROUP
3. REPORT TITLE ATMOSPHERIC MODELS FOR USE IN HYDRODYNAMIC COMPUTER CODES		
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) 1 August 1964-1 September 1964.		
5. AUTHOR(S) (Last name, first name, initial) Brackbill, Jeremiah U., Lt, USAF; Nawrocki, Edmund A., Capt, USAF; Whitaker, William A., Maj, USAF		
6. REPORT DATE August 1967	7a. TOTAL NO. OF PAGES 38	7b. NO. OF REFS 4
8a. CONTRACT OR GRANT NO.	9a. ORIGINATOR'S REPORT NUMBER(S) AFWL-TR-67-75	
a. PROJECT NO. 5710		
c. Task No. 571007K	9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
d. Subtask No. 07.002		
10. AVAILABILITY/LIMITATION NOTICES This document is subject to special export controls and each transmittal to foreign governments or foreign nationals may be made only with prior approval of AFWL (WLRT), Kirtland AFB, NM, 87117. Distribution is limited because of the technology discussed in the report.		
11. SUPPLEMENTARY NOTES (Distribution Limitation Statement No. 2)		12. SPONSORING MILITARY ACTIVITY AFWL (WLRT) Kirtland AFB, NM 87117
13. ABSTRACT A hydrostatically stable atmospheric model is necessary to perform theoretical calculations of hydrodynamic motion in the atmosphere, on a digital computer. This report presents three such models developed at the Air Force Weapons Laboratory for use in its hydrodynamic computer codes. One is for the annual mean temperate atmosphere (45° N latitude); one for the annual mean tropical atmosphere (15° N latitude); and one for the summer subarctic atmosphere (60° N latitude). The models are presented herein in tabular form and as FORTRAN subroutines which could be placed directly into any hydrodynamic computer code. For a given altitude (cm), the subroutines return a pressure (dynes/cm <sup>2</sup> ), density (gms/cm <sup>3</sup> ), specific internal energy (ergs/gm), temperature (°K), and (γ - 1). The pressures and densities agree with tabulated values to at least 1 part in 10 <sup>8</sup> and temperatures to at least 1 part in 100. The atmospheres experience an acceleration of no more than 3 parts in 10 <sup>3</sup> in a first order finite difference scheme with a zone size of 1 kilometer, the worst case.		

DD FORM 1 JAN 64 1473

UNCLASSIFIED  
Security Classification

**UNCLASSIFIED**  
Security Classification

14.	KEY WORDS	LINK A		LINK B		LINK C	
		ROLE	WT	ROLE	WT	ROLE	WT
	Temperate Atmospheric Model Tropical Atmospheric Model Subarctic Atmospheric Model						

**INSTRUCTIONS**

**1. ORIGINATING ACTIVITY:** Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.

**2a. REPORT SECURITY CLASSIFICATION:** Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

**2b. GROUP:** Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

**3. REPORT TITLE:** Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

**4. DESCRIPTIVE NOTES:** If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

**5. AUTHOR(S):** Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

**6. REPORT DATE:** Enter the date of the report as day, month, year, or month, year. If more than one date appears on the report, use date of publication.

**7a. TOTAL NUMBER OF PAGES:** The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

**7b. NUMBER OF REFERENCES:** Enter the total number of references cited in the report.

**8a. CONTRACT OR GRANT NUMBER:** If appropriate, enter the applicable number of the contract or grant under which the report was written.

**8b, 8c, & 8d. PROJECT NUMBER:** Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

**9a. ORIGINATOR'S REPORT NUMBER(S):** Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

**9b. OTHER REPORT NUMBER(S):** If the report has been assigned any other report numbers (*either by the originator or by the sponsor*), also enter this number(s).

**10. AVAILABILITY/LIMITATION NOTICES:** Enter any limitations on further dissemination of the report, other than those

imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through \_\_\_\_\_."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through \_\_\_\_\_."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through \_\_\_\_\_."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

**11. SUPPLEMENTARY NOTES:** Use for additional explanatory notes.

**12. SPONSORING MILITARY ACTIVITY:** Enter the name of the departmental project office or laboratory sponsoring (*paying for*) the research and development. Include address.

**13. ABSTRACT:** Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

**14. KEY WORDS:** Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, rules, and weights is optional.